

LAMPIRAN A
PERHITUNGAN MOISTURE CONTENT (MC)

Formula -1			
W (g)	Wp (g)	Wa (g)	MC (%)
0,5532	0,5376	0,0156	2,90
0,5413	0,5243	0,0170	3,24
0,5406	0,5221	0,0185	3,54

$3,23 \pm 0,32$

Formula a			
W (g)	Wp (g)	Wa (g)	MC (%)
0,8848	0,8543	0,0305	3,57
0,8873	0,8557	0,0316	3,69
0,8906	0,8592	0,0314	3,65

$3,64 \pm 0,06$

Formula b			
W (g)	Wp (g)	Wa (g)	MC (%)
1,1354	1,0695	0,0659	6,16
1,1382	1,0722	0,0660	6,15
1,1376	1,0712	0,0664	6,20

$6,17 \pm 0,03$

Formula ab			
W (g)	Wp (g)	Wa (g)	MC (%)
1,4450	1,3542	0,0908	6,70
1,4671	1,3752	0,0919	6,68
1,4211	1,3298	0,0913	6,86
6,75 $\pm$ 0,10			

Keterangan :

W = berat mula-mula

Wp = berat kering (setelah dioven 100 $\pm$ 2⁰ C selama 6 jam)

Wa = selisih antara W dan Wp

$$MC = \frac{Wa}{Wp} \times 100\%$$

LAMPIRAN B
HASIL UJI ANOVA MOISTURE CONTENT

Anova: Single Factor

SUMMARY

<i>Groups</i>	<i>Count</i>	<i>Sum</i>	<i>Average</i>	<i>Variance</i>
Column 1	3	9,68	3,226667	0,102533
Column 2	3	10,91	3,636667	0,003733
Column 3	3	18,51	6,17	0,0007
Column 4	3	20,24	6,746667	0,009733

ANOVA

<i>Source of Variation</i>	<i>SS</i>	<i>df</i>	<i>MS</i>	<i>F</i>	<i>P-value</i>	<i>F crit</i>
Between Groups	28,2331	3	9,411033	322,5718	1,11E-08	4,066181
Within Groups	0,2334	8	0,029175			
Total	28,4665	11				

HSD = 0,34503

	Mean	F -1	F a	F b	F ab
	3,226667	3,226667	3,636667	6,17	6,746667
F -1	3,226667	0	0,41	2,943333 *	3,52 *
F a	3,636667		0	2,533333 *	3,11 *
F b	6,17			0	0,576667
F ab	6,746667				0

LAMPIRAN C
PERHITUNGAN *FOLDING ENDURANCE*

Data Folding Endurance

Formula	Replikasi 1	Replikasi 2	Replikasi 3	Rata-rata
-l	137	135	134	135,33 $\pm$ 1,53
a	134	137	132	134,33 $\pm$ 2,52
b	164	162	163	163,00 $\pm$ 1,00
ab	166	163	165	164,67 $\pm$ 1,53

LAMPIRAN D
HASIL UJI ANOVA *FOLDING ENDURANCE*

Anova: Single Factor

SUMMARY

<i>Groups</i>	<i>Count</i>	<i>Sum</i>	<i>Average</i>	<i>Variance</i>
Column 1	3	406	135,3333	2,333333
Column 2	3	403	134,3333	6,333333
Column 3	3	489	163	1
Column 4	3	494	164,6667	2,333333

ANOVA

<i>Source of Variation</i>	<i>SS</i>	<i>df</i>	<i>MS</i>	<i>F</i>	<i>P-value</i>	<i>F crit</i>
Between Groups	2528,667	3	842,8889	280,963	1,92E-08	4,066181
Within Groups	24	8	3			
Total	2552,667	11				

HSD = 3,498743

		F -1	F a	F b	F ab	
	Mean	135,3333	134,3333	163	164,6667	
F -1	135,3333	0	-1	27,66667 *	29,33333 *	
F a	134,3333		0	28,66667 *	30,33333 *	
F b	163			0	1,666667	
F ab	164,6667				0	

LAMPIRAN E
PERHITUNGAN STATISTIK KURVA BAKU

Data Kurva Baku Natrium Diklofenak dalam Larutan Dapar Fosfat Isotonis
pH 7,4 Pengujian I

Konsentrasi (ppm)	Absorbansi	X ²	Y ²	XY
3,012	0,104	9,0721	0,0108	0,3132
6,024	0,209	36,2886	0,0437	1,2590
10,04	0,310	100,8016	0,0961	3,1124
14,056	0,469	197,5711	0,2200	6,5923
18,072	0,564	326,5972	0,3181	10,1926
22,088	0,680	487,8797	0,4624	15,0198
28,112	0,808	790,2845	0,6529	22,7145
		$\Sigma = 1948,4948$	$\Sigma = 1,8040$	$\Sigma = 59,2038$

Data Kurva Baku Natrium Diklofenak dalam Larutan Dapar Fosfat Isotonis
pH 7,4 Pengujian II

Konsentrasi (ppm)	Absorbansi	X ²	Y ²	XY
3,018	0,09	9,1083	0,0081	0,2716
6,036	0,21	36,4333	0,0441	1,2676
10,06	0,322	101,2036	0,1037	3,2393
14,084	0,46	198,3590	0,2116	6,4786
18,108	0,57	327,8997	0,3249	10,3216
22,132	0,697	489,8254	0,4858	15,4260
28,168	0,825	793,4362	0,6806	23,2386
		$\Sigma = 1956,2655$	$\Sigma = 1,8588$	$\Sigma = 60,2433$

Data Kurva Baku Natrium Diklofenak dalam Larutan Dapar Fosfat Isotonis
pH 7,4 Pengujian III

Konsentrasi (ppm)	Absorbansi	X ²	Y ²	XY
3,03	0,095	9,1809	0,0090	0,2878
6,06	0,226	36,7236	0,0511	1,3696
10,1	0,336	102,01	0,1129	3,3936
14,14	0,456	199,9396	0,2079	6,4478
18,18	0,584	330,5124	0,3410	10,6171
22,22	0,675	493,7284	0,4556	14,9985
28,28	0,810	799,7584	0,6561	22,9068
		$\Sigma = 1971,8533$	$\Sigma = 1,8336$	$\Sigma = 60,0212$

	ΣX^2	ΣXY	ΣY^2	N	SSi	RDF
I	1948,4948	59,2038	1,8040	7	1,7735	6
II	1956,2655	60,2433	1,8588	7	1,8280	6
III	1971,8533	60,0212	1,8336	7	1,8225	6
	5876,6136	179,4683	5,4964		5,4241	

$$SSc = \Sigma Yc - [(\Sigma Xyc)^2 / \Sigma Xc]$$

$$= 5,4964 - [179,4683 / 5876,6136]$$

$$= 5,465910568$$

$$SSp = SS1 + SS2 + SS3$$

$$= 1,7735 + 1,8280 + 1,8225$$

$$= 5,4241$$

$$F_{hitung} = (SSc - SSp / k - 1) / (SSp / 12)$$

$$= (5,465910568 - 5,4241 / 3 - 1) / (5,4241 / 18) = 0,0694$$

$$F_{hitung} < F_{tabel} 0,05 (2 : 18) = 3,63$$

LAMPIRAN F
PERHITUNGAN AKURASI PRESISI

Replikasi	%	Abs	C (ppm)	C Teoritis (ppm)	% Perolehan Kembali
1	80	0,215	6,416	6,400	100,24
	100	0,263	8,046	8,000	100,58
	120	0,312	9,711	9,600	101,15
2	80	0,213	6,348	6,400	99,18
	100	0,266	8,148	8,000	101,85
	120	0,308	9,575	9,600	99,74
3	80	0,216	6,449	6,400	100,77
	100	0,262	8,012	8,000	100,15
	120	0,314	9,779	9,600	101,86
$\bar{x}$ (%) $\pm$ SD					100,61 $\pm$ 0,91
SD rel (%)					0,90

Contoh Perhitungan :

Absorbansi = 0,215 $\longrightarrow$ $y = 0,0294x + 0,0261$

C sebenarnya = 6,416 ppm

C teoritis = 6,400 ppm

% perolehan kembali = $(C \text{ sebenarnya} / C \text{ teoritis}) \times 100 \%$

$$= (6,416 / 6,400) \times 100 \%$$

$$= 100,24 \%$$

$$\% \text{ KV} = \frac{SD}{\bar{x}} \times 100\%$$

$$= \frac{0,91}{100,61} \times 100\% = 0,90$$

LAMPIRAN G
PERHITUNGAN PENETAPAN KADAR

F	Uji	Abs	C (ppm)	C (mg/cm² <i>patch</i>)	$\bar{x} \pm SD$	SD rel (%)
-1	1	0,264	8,092	0,404	$0,4057 \pm 0,0047$	1,16
	2	0,268	8,216	0,411		
	3	0,263	8,046	0,402		
a	1	0,266	8,148	0,407	$0,4090 \pm 0,0062$	1,53
	2	0,271	8,318	0,416		
	3	0,264	8,080	0,404		
b	1	0,272	8,364	0,418	$0,410 \pm 0,0075$	1,83
	2	0,263	8,058	0,403		
	3	0,267	8,194	0,410		
ab	1	0,267	8,194	0,410	$0,406 \pm 0,0045$	1,11
	2	0,265	8,126	0,406		
	3	0,262	8,024	0,401		

Contoh Perhitungan :

Absorbansi = 0,264 $\longrightarrow y = 0,0294x + 0,0261$

C = 8,092 ppm $\longrightarrow 8,092 \mu\text{g/ml} \times 50 \text{ ml} = 404,6 \mu\text{g} = 0,404 \text{ mg/cm}^2$
patch

LAMPIRAN H
HASIL UJI ANOVA PENETAPAN KADAR

Anova: Single Factor

SUMMARY

<i>Groups</i>	<i>Count</i>	<i>Sum</i>	<i>Average</i>	<i>Variance</i>
Column 1	3	1,217	0,405667	2,23E-05
Column 2	3	1,227	0,409	3,9E-05
Column 3	3	1,231	0,410333	5,63E-05
Column 4	3	1,217	0,405667	2,03E-05

ANOVA

<i>Source of Variation</i>	<i>SS</i>	<i>df</i>	<i>MS</i>	<i>F</i>	<i>P-value</i>	<i>F crit</i>
Between Groups	5,07E-05	3	1,69E-05	0,489533	0,699152	4,066181
Within Groups	0,000276	8	3,45E-05			
Total	0,000327	11				

LAMPIRAN I

ANALISA FAKTORIAL DESAIN PELEPASAN

Use your mouse to right click on individual cells for definitions.

Response 1 Pelepasan

ANOVA for selected factorial model

Analysis of variance table [Partial sum of squares - Type III]

Source	Sum of Squares	Mean Square	F Value	p-value Prob > F
Model	2089.52	696.51	1642.77	< 0.0001
significant				
<i>A-HPMC</i>	<i>1771.03</i>	<i>1771.03</i>	<i>4177.13</i>	<i>< 0.0001</i>
<i>B-Asam oleat</i>	<i>303.03</i>	<i>303.03</i>	<i>714.72</i>	<i>< 0.0001</i>
<i>AB</i>	<i>15.46</i>	<i>15.46</i>	<i>36.47</i>	<i>0.0003</i>
Pure Error	3.39	0.42		
Cor Total	2092.92			

The Model F-value of 1642.77 implies the model is significant. There is only a 0.01% chance that a "Model F-Value" this large could occur due to noise.

Values of "Prob > F" less than 0.0500 indicate model terms are significant.

In this case A, B, AB are significant model terms.

Values greater than 0.1000 indicate the model terms are not significant.

If there are many insignificant model terms (not counting those required to support hierarchy), model reduction may improve your model.

The "Pred R-Squared" of 0.9964 is in reasonable agreement with the "Adj R-Squared" of 0.9978.

"Adeq Precision" measures the signal to noise ratio. A ratio greater than 4 is desirable. Your ratio of 91.365 indicates an adequate signal. This model can be used to navigate the design space.

Final Equation in Terms of Coded Factors:

$$\begin{aligned} \text{Pelepasan} &= \\ &+107.06 \\ &-12.15 * A \\ &+5.03 * B \\ &+1.14 * A * B \end{aligned}$$

Final Equation in Terms of Actual Factors:

$$\begin{aligned} \text{Pelepasan} &= \\ &+107.05817 \\ &-12.14850 * \text{HPMC} \\ &+5.02517 * \text{Asam oleat} \\ &+1.13517 * \text{HPMC} * \text{Asam oleat} \end{aligned}$$

The Diagnostics Case Statistics Report has been moved to the Diagnostics Node. In the Diagnostics Node, Select Case Statistics from the View Menu.

Proceed to Diagnostic Plots (the next icon in progression). Be sure to look at the:

- 1) Normal probability plot of the studentized residuals to check for normality of residuals.
- 2) Studentized residuals versus predicted values to check for constant error.
- 3) Externally Studentized Residuals to look for outliers, i.e., influential values.

- 4) Box-Cox plot for power transformations.
If all the model statistics and diagnostic plots are OK, finish up
with the Model Graphs icon.



LAMPIRAN J
ANALISA FAKTORIAL DESAIN PENETRASI

Response 2 Penetrasi

ANOVA for selected factorial model

Analysis of variance table [Partial sum of squares - Type III]

Source	Sum of Squares	Mean Square	F Value	p-value Prob > F
Model	526.69	175.56	2097.33	< 0.0001
significant				
<i>A-HPMC</i>	<i>306.61</i>	<i>306.61</i>	<i>3662.82</i>	<i>< 0.0001</i>
<i>B-Asam oleat</i>	<i>220.03</i>	<i>220.03</i>	<i>2628.61</i>	<i>< 0.0001</i>
<i>AB</i>	<i>0.047</i>	<i>0.047</i>	<i>0.56</i>	<i>0.4774</i>
Pure Error	0.67	0.084		
Cor Total	527.36			

The Model F-value of 2097.33 implies the model is significant. There is only a 0.01% chance that a "Model F-Value" this large could occur due to noise.

Values of "Prob > F" less than 0.0500 indicate model terms are significant.

In this case A, B are significant model terms.

Values greater than 0.1000 indicate the model terms are not significant.

If there are many insignificant model terms (not counting those required to support hierarchy),

model reduction may improve your model.

The "Pred R-Squared" of 0.9971 is in reasonable agreement with the "Adj R-Squared" of 0.9983.

"Adeq Precision" measures the signal to noise ratio. A ratio greater than 4 is desirable. Your ratio of 111.791 indicates an adequate signal. This model can be used to navigate the design space.

Final Equation in Terms of Coded Factors:

$$\begin{aligned} \text{Penetrasi} &= \\ &+29.72 \\ &-5.05 * A \\ &+4.28 * B \\ &-0.062 * A * B \end{aligned}$$

Final Equation in Terms of Actual Factors:

$$\begin{aligned} \text{Penetrasi} &= \\ &+29.71558 \\ &-5.05475 * \text{HPMC} \\ &+4.28208 * \text{Asam oleat} \\ &-0.062250 * \text{HPMC} * \text{Asam oleat} \end{aligned}$$

The Diagnostics Case Statistics Report has been moved to the Diagnostics Node.

In the Diagnostics Node, Select Case Statistics from the View Menu. Proceed to Diagnostic Plots (the next icon in progression). Be sure to look at the:

- 1) Normal probability plot of the studentized residuals to check for normality of residuals.
- 2) Studentized residuals versus predicted values to check for constant error.

- 3) Externally Studentized Residuals to look for outliers, i.e., influential values.
- 4) Box-Cox plot for power transformations.
- If all the model statistics and diagnostic plots are OK, finish up with the Model Graphs icon.



LAMPIRAN K

TABEL UJI r

Tabel Korelasi (r)

DEGREES OF FREEDOM (DF)	5 PERCENT	1 PERCENT	DEGREES OF FREEDOM (DF)	5 PERCENT	1 PERCENT
1	.997	1.000	24	.388	.496
2	.950	.990	25	.381	.487
3	.878	.959	26	.374	.478
4	.811	.917	27	.367	.470
5	.754	.874	28	.361	.463
6	.707	.834	29	.355	.456
7	.666	.798	30	.349	.449
8	.632	.765	35	.325	.418
9	.602	.735	40	.304	.393
10	.576	.708	48	.288	.372
11	.553	.684	50	.273	.354
12	.532	.661	60	.250	.325
13	.514	.641	70	.232	.302
14	.497	.623	80	.217	.283
15	.482	.606	90	.205	.267
16	.468	.590	100	.195	.254
17	.456	.575	125	.174	.228
18	.444	.561	150	.159	.208
19	.433	.549	200	.138	.181
20	.423	.537	300	.113	.148
21	.413	.526	400	.098	.128
22	.404	.515	500	.088	.115
23	.396	.505	1000	.062	.081

Sumber: Soedigdo & Soedigdo (1977)

LAMPIRAN L

TABEL UJI F

Tabel uji F

Basis pertama pada setiap pasangan baris adalah titik pada distribusi F untuk aras 0.05; baris kedua untuk aras 0.01.

		Derajat kebebasan untuk rataan kuadrat yang lebih besar																										
		1	2	3	4	5	6	7	8	9	10	11	12	14	16	20	24	30	40	50	75	100	200	500	∞			
Derajat kebebasan untuk rataan kuadrat yang lebih kecil.	16	4.49 8.53	3.63 6.23	3.24 5.29	3.01 4.77	2.85 4.44	2.74 4.20	2.66 4.03	2.59 3.89	2.54 3.78	2.49 3.69	2.45 3.61	2.42 3.55	2.37 3.45	2.33 3.37	2.28 3.25	2.24 3.18	2.20 3.10	2.16 3.01	2.13 2.96	2.09 2.89	2.07 2.86	2.04 2.80	2.02 2.77	2.01 2.75			
	17	4.45 8.40	3.59 6.11	3.20 5.18	2.96 4.67	2.81 4.34	2.70 4.10	2.62 3.93	2.55 3.79	2.50 3.68	2.45 3.59	2.41 3.52	2.38 3.45	2.33 3.35	2.29 3.27	2.23 3.16	2.19 3.08	2.15 3.00	2.11 2.92	2.08 2.84	2.04 2.79	2.02 2.76	1.99 2.70	1.97 2.67	1.96 2.65			
	18	4.41 8.36	3.55 6.01	3.16 5.09	2.92 4.58	2.77 4.25	2.66 4.01	2.58 3.85	2.51 3.71	2.46 3.60	2.41 3.51	2.37 3.44	2.34 3.37	2.29 3.27	2.25 3.19	2.19 3.07	2.15 3.00	2.11 2.91	2.07 2.83	2.04 2.78	2.00 2.71	1.98 2.68	1.95 2.62	1.93 2.59	1.92 2.57			
	19	4.38 8.18	3.52 5.93	3.13 5.01	2.90 4.50	2.74 4.17	2.63 3.94	2.55 3.77	2.48 3.63	2.43 3.52	2.38 3.43	2.34 3.36	2.31 3.30	2.26 3.19	2.21 3.12	2.15 3.00	2.11 2.92	2.07 2.84	2.02 2.76	2.00 2.70	1.96 2.63	1.94 2.60	1.91 2.54	1.90 2.51	1.88 2.49			
	20	4.35 8.10	3.49 5.85	3.10 4.94	2.87 4.43	2.71 4.10	2.60 3.87	2.52 3.71	2.45 3.56	2.40 3.45	2.35 3.37	2.31 3.30	2.28 3.23	2.23 3.13	2.18 3.05	2.12 2.94	2.08 2.86	2.04 2.77	1.99 2.69	1.96 2.63	1.92 2.56	1.90 2.53	1.87 2.47	1.85 2.44	1.84 2.42			
	21	4.32 8.02	3.47 5.78	3.07 4.87	2.84 4.37	2.68 4.04	2.57 3.81	2.49 3.65	2.42 3.51	2.37 3.40	2.32 3.31	2.28 3.24	2.25 3.17	2.20 3.07	2.15 2.99	2.09 2.88	2.05 2.80	2.00 2.73	1.96 2.67	1.93 2.63	1.90 2.51	1.87 2.47	1.84 2.42	1.82 2.37	1.81 2.33	1.81 2.31		
	22	4.30 7.94	3.44 5.72	3.05 4.82	2.82 4.31	2.66 3.99	2.55 3.76	2.47 3.59	2.40 3.45	2.35 3.35	2.30 3.26	2.26 3.18	2.23 3.12	2.18 3.02	2.13 2.94	2.07 2.83	2.03 2.75	1.98 2.67	1.93 2.58	1.91 2.53	1.87 2.46	1.84 2.42	1.81 2.37	1.80 2.33	1.79 2.31			
	23	4.28 7.88	3.42 5.66	3.03 4.76	2.80 4.26	2.64 3.94	2.53 3.71	2.45 3.54	2.38 3.41	2.32 3.30	2.28 3.21	2.24 3.14	2.20 3.07	2.14 2.97	2.10 2.89	2.04 2.78	2.00 2.70	1.96 2.62	1.91 2.53	1.88 2.48	1.84 2.41	1.82 2.37	1.79 2.32	1.77 2.28	1.76 2.25			
	24	4.26 7.82	3.40 5.61	3.01 4.72	2.78 4.22	2.62 3.90	2.51 3.67	2.43 3.50	2.36 3.36	2.30 3.25	2.26 3.17	2.22 3.09	2.18 3.03	2.13 2.93	2.09 2.85	2.02 2.74	1.98 2.66	1.94 2.58	1.89 2.49	1.86 2.44	1.82 2.36	1.80 2.33	1.76 2.27	1.74 2.23	1.73 2.21			
	25	4.24 7.77	3.38 5.57	2.99 4.68	2.76 4.18	2.60 3.86	2.49 3.63	2.41 3.46	2.34 3.32	2.28 3.21	2.24 3.13	2.20 3.05	2.16 2.99	2.11 2.89	2.06 2.81	2.00 2.70	1.96 2.62	1.92 2.54	1.87 2.45	1.84 2.40	1.80 2.32	1.77 2.29	1.74 2.23	1.72 2.19	1.71 2.17			
	26	4.22 7.72	3.37 5.53	2.89 4.64	2.74 4.14	2.59 3.82	2.47 3.59	2.39 3.42	2.32 3.29	2.27 3.17	2.22 3.09	2.18 3.02	2.15 2.96	2.10 2.86	2.05 2.77	1.99 2.66	1.95 2.58	1.90 2.50	1.85 2.41	1.82 2.36	1.78 2.28	1.76 2.25	1.72 2.19	1.70 2.15	1.69 2.13			
	27	4.21 7.68	3.35 5.49	2.96 4.60	2.73 4.11	2.57 3.79	2.46 3.56	2.37 3.39	2.30 3.26	2.25 3.14	2.20 3.06	2.16 2.98	2.13 2.93	2.08 2.83	2.03 2.74	1.97 2.63	1.93 2.55	1.88 2.47	1.84 2.38	1.80 2.33	1.76 2.25	1.74 2.21	1.71 2.18	1.68 2.13	1.67 2.10			
	28	4.20 7.64	3.34 5.45	2.95 4.57	2.71 4.07	2.56 3.76	2.44 3.53	2.36 3.36	2.29 3.23	2.24 3.11	2.19 3.03	2.15 2.95	2.12 2.90	2.06 2.80	2.02 2.71	1.96 2.60	1.91 2.52	1.87 2.44	1.81 2.35	1.78 2.30	1.75 2.22	1.72 2.18	1.69 2.13	1.67 2.09	1.65 2.06			
	29	4.18 7.60	3.33 5.52	2.93 4.54	2.70 4.04	2.54 3.73	2.43 3.50	2.35 3.32	2.28 3.20	2.22 3.08	2.18 3.00	2.14 2.92	2.10 2.87	2.05 2.77	2.00 2.68	1.94 2.57	1.89 2.49	1.85 2.41	1.80 2.32	1.77 2.27	1.73 2.19	1.71 2.15	1.68 2.10	1.65 2.06	1.64 2.03			
	30	4.17 7.56	3.32 5.39	2.92 4.51	2.69 4.02	2.53 3.70	2.42 3.47	2.34 3.30	2.27 3.17	2.21 3.06	2.16 2.98	2.12 2.90	2.09 2.84	2.04 2.74	1.99 2.66	1.93 2.53	1.89 2.47	1.84 2.38	1.79 2.29	1.76 2.24	1.72 2.16	1.69 2.13	1.66 2.07	1.64 2.03	1.62 2.01			

(bersambung)

Tabel Uji F (lanjutan)

Tabel uji F (lanjutan)

Baris pertama pada setiap pasangan baris adalah titik pada distribusi F untuk aras 0.05; baris kedua untuk aras 0.01.

		Derajat kebebasan untuk rataan kuadrat yang lebih besar.																									
		1	2	3	4	5	6	7	8	9	10	11	12	14	16	20	24	30	40	50	75	100	200	500	∞		
Derajat kebebasan untuk rataan kuadrat yang lebih kecil.	32	4.15 7.50	3.30 5.34	2.90 4.46	2.67 3.97	2.51 3.66	2.40 3.42	2.32 3.25	2.25 3.12	2.19 3.01	2.14 2.94	2.10 2.86	2.07 2.80	2.02 2.70	1.97 2.62	1.91 2.51	1.86 2.42	1.82 2.34	1.76 2.25	1.74 2.20	1.69 2.12	1.67 2.08	1.64 2.02	1.61 1.98	1.59 1.96		
	34	4.13 7.44	3.28 5.29	2.88 4.42	2.65 3.93	2.49 3.61	2.38 3.38	2.30 3.21	2.23 3.08	2.17 2.97	2.12 2.89	2.08 2.82	2.05 2.76	2.00 2.66	1.95 2.58	1.89 2.47	1.84 2.38	1.80 2.30	1.74 2.21	1.71 2.15	1.67 2.08	1.64 2.04	1.61 1.98	1.59 1.94	1.57 1.91		
	36	4.11 7.39	3.26 5.25	2.86 4.38	2.63 3.89	2.48 3.58	2.36 3.35	2.28 3.18	2.21 3.04	2.15 2.94	2.10 2.86	2.06 2.78	2.03 2.72	1.99 2.62	1.93 2.54	1.87 2.43	1.82 2.35	1.78 2.26	1.72 2.17	1.69 2.12	1.65 2.04	1.62 2.00	1.59 1.94	1.56 1.90	1.55 1.87		
	38	4.10 7.36	3.25 5.21	2.85 4.34	2.62 3.86	2.46 3.54	2.35 3.32	2.26 3.15	2.19 3.02	2.14 2.91	2.09 2.82	2.05 2.75	2.02 2.69	1.96 2.59	1.92 2.51	1.85 2.40	1.80 2.32	1.76 2.22	1.71 2.14	1.67 2.08	1.63 2.00	1.60 1.97	1.57 1.90	1.54 1.86	1.53 1.84		
	40	4.08 7.31	3.23 5.18	2.84 4.31	2.61 3.83	2.45 3.51	2.34 3.29	2.25 3.12	2.18 2.99	2.12 2.88	2.07 2.80	2.04 2.73	2.00 2.66	1.95 2.56	1.90 2.49	1.84 2.37	1.79 2.29	1.74 2.20	1.69 2.11	1.66 2.05	1.61 1.97	1.59 1.94	1.55 1.88	1.53 1.84	1.51 1.81		
	42	4.07 7.27	3.22 5.15	2.83 4.29	2.59 3.80	2.44 3.49	2.32 3.26	2.24 3.10	2.17 2.96	2.11 2.86	2.06 2.77	2.02 2.70	1.99 2.64	1.94 2.54	1.89 2.46	1.82 2.35	1.78 2.26	1.73 2.17	1.68 2.08	1.64 2.02	1.60 1.94	1.57 1.91	1.54 1.85	1.51 1.80	1.49 1.78		
	44	4.06 7.24	3.21 5.12	2.82 4.26	2.58 3.78	2.43 3.46	2.31 3.24	2.23 3.07	2.16 2.94	2.10 2.84	2.05 2.75	2.01 2.68	1.98 2.62	1.92 2.52	1.88 2.44	1.81 2.32	1.76 2.24	1.72 2.15	1.66 2.06	1.63 2.09	1.58 1.92	1.56 1.88	1.52 1.82	1.50 1.78	1.48 1.75		
	46	4.05 7.21	3.20 5.10	2.81 4.24	2.57 3.76	2.42 3.44	2.30 3.22	2.22 3.05	2.14 2.92	2.09 2.82	2.04 2.73	2.00 2.66	1.97 2.60	1.91 2.50	1.87 2.42	1.80 2.30	1.75 2.22	1.71 2.13	1.65 2.04	1.62 1.98	1.57 1.90	1.54 1.86	1.51 1.80	1.48 1.76	1.46 1.72		
	48	4.04 7.19	3.19 5.08	2.80 4.22	2.56 3.74	2.41 3.42	2.30 3.20	2.21 3.04	2.14 2.90	2.08 2.80	2.03 2.71	1.99 2.64	1.96 2.58	1.90 2.48	1.86 2.40	1.79 2.28	1.74 2.20	1.70 2.11	1.64 2.02	1.61 1.96	1.56 1.88	1.53 1.84	1.50 1.78	1.47 1.73	1.45 1.70		
	50	4.03 7.17	3.18 5.06	2.79 4.20	2.56 3.72	2.40 3.41	2.29 3.18	2.20 3.02	2.13 2.88	2.07 2.78	2.02 2.70	1.98 2.62	1.95 2.56	1.90 2.46	1.85 2.39	1.78 2.26	1.74 2.18	1.69 2.10	1.63 2.00	1.60 1.94	1.55 1.86	1.52 1.82	1.48 1.76	1.46 1.71	1.44 1.68		
	55	4.02 7.12	3.17 5.01	2.78 4.16	2.54 3.68	2.38 3.37	2.27 3.15	2.18 3.10	2.11 2.96	2.05 2.85	2.00 2.75	1.97 2.66	1.93 2.59	1.88 2.53	1.83 2.43	1.76 2.35	1.72 2.23	1.67 2.15	1.61 2.04	1.58 1.96	1.52 1.90	1.50 1.82	1.46 1.78	1.43 1.71	1.41 1.66		
	60	4.00 7.08	3.15 4.98	2.76 4.13	2.52 3.65	2.37 3.34	2.25 3.12	2.17 2.95	2.10 2.82	2.04 2.72	1.99 2.63	1.95 2.56	1.92 2.40	1.86 2.32	1.81 2.20	1.75 2.12	1.70 2.03	1.65 1.93	1.59 1.87	1.56 1.79	1.50 1.74	1.48 1.68	1.44 1.63	1.41 1.60	1.39 1.58		
	65	3.99 7.04	3.14 4.95	2.75 4.10	2.51 3.62	2.36 3.31	2.24 3.09	2.15 2.93	2.08 2.79	2.02 2.70	1.98 2.61	1.94 2.54	1.90 2.47	1.85 2.37	1.80 2.20	1.73 2.09	1.68 2.00	1.63 1.90	1.57 1.84	1.54 1.76	1.49 1.71	1.46 1.64	1.42 1.60	1.39 1.56	1.37 1.54		
	70	3.98 7.01	3.13 4.92	2.74 4.08	2.50 3.60	2.35 3.29	2.32 3.07	2.14 2.91	2.07 2.77	2.01 2.67	1.97 2.59	1.93 2.51	1.89 2.45	1.84 2.35	1.79 2.25	1.72 2.07	1.67 1.99	1.62 1.88	1.56 1.82	1.53 1.74	1.47 1.69	1.45 1.62	1.40 1.56	1.37 1.53	1.35 1.51		
	80	3.96 6.96	3.11 4.88	2.72 4.04	2.48 3.56	2.33 3.25	2.21 3.04	2.12 2.87	2.05 2.74	1.99 2.64	1.95 2.55	1.91 2.48	1.88 2.41	1.82 2.32	1.77 2.24	1.70 2.11	1.65 2.03	1.60 1.94	1.54 1.84	1.51 1.78	1.45 1.70	1.42 1.65	1.38 1.57	1.35 1.52	1.32 1.49		

Sumber: Scheffler (1987).